

OPEN ACCESS

Editors' Choice—Methods—Pressure Control Apparatus for Lithium **Metal Batteries**

To cite this article: Bingyu Lu et al 2022 J. Electrochem. Soc. 169 070537

View the article online for updates and enhancements.



ECS Membership = Connection

ECS membership connects you to the electrochemical community:

Visit electrochem.org/join

• Facilitate your research and discovery through ECS meetings which convene scientists from around the world;

- Access professional support through your lifetime career:
- Open up mentorship opportunities across the stages of your career;
- Build relationships that nurture partnership, teamwork—and success!

with your community

This content was downloaded from IP address 207.242.19.75 on 29/07/2022 at 19:22

Join ECS!





Editors' Choice—Methods—Pressure Control Apparatus for Lithium Metal Batteries

Bingyu Lu,¹ Wurigumula Bao,¹^(b) Weiliang Yao,² Jean-Marie Doux,¹ Chengcheng Fang,^{3,2}^(b) and Ying Shirley Meng^{1,4,2}^(b)

¹Department of NanoEngineering, University of California San Diego, La Jolla, California 92093, United States of America ²Materials Science and Engineering, University of California San Diego, La Jolla, California 92093, United States of America

³Department of Chemical Engineering and Materials Science, Michigan State University, East Lansing, Michigan 48824, United States of America

⁴Pritzker School of Molecular Engineering, The University of Chicago, Chicago, Illinois 60637, United States of America

Lithium (Li) metal anodes are essential for developing next-generation high-energy-density batteries. However, Li dendrite/ whisker formation caused short-circuiting issue and short cycle life have prevented lithium metal from being viably used in rechargeable batteries. Numerous works have been done to study how to regulate the Li growth in electrochemical cycling by using external stacking forces. While it is widely agreed that stack pressure positively affects the lithium plating/stripping process, the optimized pressure range provided by different works varies greatly because of the difference in the pressure control setup. In this work, a pressure control apparatus is designed for Li metal batteries with liquid and solid-state electrolytes (SSE). With considerations of minimizing cell to cell variation, a reusable split cell and pressure load cell are made for testing electrochemical culls with high precision pressure control. The capability of the designed setup is demonstrated by studying the pressure effect on the Li plating/stripping process.

© 2022 The Author(s). Published on behalf of The Electrochemical Society by IOP Publishing Limited. This is an open access article distributed under the terms of the Creative Commons Attribution 4.0 License (CC BY, http://creativecommons.org/licenses/by/4.0/), which permits unrestricted reuse of the work in any medium, provided the original work is properly cited. [DOI: 10.1149/1945-7111/ac834c]

Manuscript submitted April 18, 2022; revised manuscript received July 7, 2022. Published July 29, 2022.

The world has witnessed tremendous development in portable electronic devices and electric vehicle technology over the last four decades.^{1,2} With its high theoretical capacity (3,860 mAh g⁻¹ . or 2,061 mAh cm⁻³) and low electrochemical potential (-3.04 V versus the standard hydrogen electrode), lithium (Li) metal has been regarded as the "Holy Grail" anode material candidate for nextgeneration batteries.^{3,4} Still, many formidable obstacles need to be overcome before Li metal could be used practically as the anode in commercial cells. The fundamental problems of using a Li metal include the continuous formation of (1) Solid Electrolyte Interphase (SEI), (2) Li dendrites/whiskers and (3) "inactive" or "dead" Li. Because of the highly negative electrochemical potential of Li⁺/Li, electrolyte components can easily decompose and form SEI on the surface of Li metal. However, the fragile structure of SEI could easily be fractured and reformed during the plating and stripping process, leading to the heterogeneous ionic conductivity of the SEI. The cracks on the SEI and the inhomogeneous ionic conductivity together cause the growth of Li dendrite.⁶ In the stripping process, the high tortuosity of the Li dendrite could easily isolate metallic Li from electron-conducting materials, causing so-called "dead" Li.⁵ The formation of the "dead" Li during the cycling eventually leads to the low Coulombic efficiency (CE) and safety hazards of the Li metal batteries.

Recently, studies have been focusing on using external mechanical force to control the growth of Li morphology in both liquid electrolytes and SSE.^{7–15} The effect of external stacking pressure was first studied by Dr Wilkinson and his colleagues in 1991.¹⁶ By designing an in situ cell, they could monitor the volume expansion and pressure evolution of the Li metal battery while it is cycling. It was discovered that mechanical pressure greatly affected the morphology of the electrochemically deposited Li (EDLi). The results indicated that at low stacking pressure (below 140 kPa), the EDLi was in a needle-like structure, while at large stacking pressure (1400 kPa), the EDLi formed a column-like structure, which was dense and uniform. They believed the improved morphology was the reason why the CE of the cell with high stacking pressure was better. Inspired by this conclusion, many

recent works have studied the importance of pressure on Li metal anode. Anode-free pouch cells with external stacking plates were mostly used to study how various pressure (0 to 2000 kPa) could affect the cyclability of the cell.¹⁷⁻²⁰ The results show that as the pressure increased, the capacity retention of the anode-free cell would generally improve. However, the amount of improvement was related to the type of cell setup, and sometimes high pressure would even hinder the cell's performance. The precise control of stack pressure on the all-solid-state battery (ASSB) is also crucial for cycling stability. Internal shorting caused by Li dendrite formation is prevalent during ASSB cycling. Porz et al. claimed that Li could penetrate even near-perfectly dense single crystal oxide solid electrolytes (such as $Li_7La_3Zr_2O_{12}$) during the cycling, leading to the shorting of the cell as a result.²¹ Doux et al. further explored the effects of the stack pressure on the cycling stability of the ASSB. It was found out that the optimized stack pressure of 5 MPa could enable Li metal anode to cycle at room temperature without shorting for more than 1000 h.¹⁵

As numerous studies have been done trying to determine the optimized pressure ranging for Li metal anode cycling, it has been brought to attention that a carefully designed pressure control setup is needed to quantitatively study the effects of pressure on the cycling behavior of lithium metal anode. In this work, a split cell coupled with a pressure load cell (a pressure sensor) is designed for precisely controlling and monitoring the stacking pressure of Li metal cells. The primary goal of using this pressure apparatus is to provide the research community a universal, standardized, prototype cell design for fundamental study on the Li metal anode systems with easy assemble and dissemble process. The small scale and single layer design can also help us to control the stack pressure with higher precision (0.1 kPa), which is essential in understanding the fundamental materials behaviors. The effect of pressure on the Li plating/stripping and full cell cycling process is also demonstrated as an example.

Pressure Control Apparatus

Split cell.—The split cell consists of two parts (Fig. 1): one polyether ether ketone (PEEK) die (Figs. 1a, 1d) mold and two titanium (Ti) plungers (Figs. 1b, 1c, 1e). The Ti plungers have dual



Figure 1. Dimensions for the split cell setup. Side views of (a) PEEK Cylinder; (b) Long Titanium Plunger; (c) Short Titanium Plunger. Top view of (d) PEEK Cylinder; (e) Titanium Plungers. (f) Complete and cross-sectional view of the split cell setup.

purposes in the split cells: (1) to work as current collectors and (2) to apply pressure. Therefore, Ti is chosen as the material for the plungers because of its high electronic conductivity, high mechanical strength, and high stability towards chemical corrosion. One hole is drilled on the bottom of the plungers to provide space for the banana plugs that are connected to the battery cyclers. The PEEK die mold is used as a container to hold the electrochemical cell in place. The total length of the Ti plungers (1.65 inches) is slightly higher than the length of the PEEK die (1.55 inches) so that the PEEK die can freely adjust its position and will not affect the pressure control. All parts require high precision machine polishing so that the friction between the Ti plunger and the inner wall of the PEEK die mold is at a minimum. If the polishing on the PEEK die mold and Ti plunger is not carefully done, extra force might be needed to overcome the friction between the two components, leading to less accurate readings from pressure load cells. Therefore, it is important that the friction between the titanium plungers and the PEEK die does not influence the pressure control while providing a good sealing for the electrochemical cell inside (Fig. 1f). Furthermore, the split cell design avoids sealing components such as o-rings. The o-ring sealing cannot guarantee completely airtightness, and will further bring uncertainty to the stack pressure value due to friction force. The current design can already provide good sealing for liquid cell cycling for a few days (Fig. 4e).

Casing.—The casing consists of two parts (Fig. 2): three threaded rods (Fig. 2a) and top/bottom plates (Fig. 2b). The split cell and the pressure load cell are placed uniaxially inside the casing (Fig. 4a). The top/bottom plates stack the split cell and the pressure load cell. Bolts or wing nuts are used to precisely control the stack pressure exerted by the plates. A thin PEEK disc is sunk into the top/ bottom plates at the center where the split cell will sit. The PEEK disc can prevent shorting. All the metal parts of the casing are made of stainless steel.

Load cell calibration.- The DYHW-116 load cell (Bengbu Dayang Sensing System Engineering Co. Ltd.) and a digital LED display monitor the exerted stacking pressure on the split cell. The load cells have different measuring ranges. Choosing the most suitable range (0 to 1000 kPa is enough for Li metal anode with liquid electrolyte) for the specific testing scenario is beneficial for a higher pressure resolution. Besides, it is crucial to calibrate the load cell before use since the default reading of the load cell might be way off from the actual pressure that is being measured. To calibrate the load cell, a set of known loads is first applied onto the load cell by using the 100 kN Instron 5982 Universal Testing System (Fig. 3a). The readings from the load cell are first calibrated at the end of the range of the load cell (i.e., 1000 kPa for the load cell described earlier). Then, the accuracy of the load cell setup can be compared to the load applied by the Instron testing system over the whole range of the load cell to ensure that the calibration is accurate. This calibration method allows to precisely set the load cell readings to the actual pressure applied to the sample by taking into account the sample area.

Example: pressure effects on the Li metal cell cycling.—With liquid electrolyte: The Cu||Li cell is assembled in an Ar-filled glovebox. The Cu||Li cell is made by sandwiching a thin Li metal foil (7 mm diameter, 50 μ m thick), Celgard 2325 separator (10 mm diameter), and the cleaned Cu foil (10 mm diameter) between the two Ti plungers inside the PEEK die mold. It is recommended to use thin Li metal foil (less than 50 μ m) in the split cell because thicker lithium foil (higher than 500 μ m) will deform significantly under high pressure, leading to a relaxation of pressure during testing or even short-circuiting. Only a minimum amount of electrolyte (~5 μ l) is required for the Cu||Li cells. After the assembly, the split cell onto the load cell and then fixed by the cell casing, which provides the uniaxial stacking pressure on the cell casing. The nuts



Figure 2. Dimensions for the casing for the split cell and load cell. (a) Side view of the casing rods and bottom; (b) Top view of the Top and Bottom of the casing.



Figure 3. (a) The calibration of the load cell using Instron 5982 Universal Testing System. (b) Zoom-in image of the load cell.

need to be carefully adjusted in order to apply the desired stacking pressure. It is important to adjust the split cell in a vertical position so that the applied pressure can be uniformly distributed.

Figure 4b demonstrates the first cycle charge-discharge profile of Li||Cu cell under different pressure with liquid electrolyte. The CE is directly related to the external pressure exerted on the cell. At 0 kPa (no external pressure, only gravitational force), the plating process shows the highest overpotential (-0.48 V), and the CE is only 82.06% even with a high concentration ether-based electrolyte.^{11,23} With a slight increase of the stacking pressure (50 kPa), the plating overpotential decreased to -0.22 V, and the CE increased to 91.41%. With the further increase of the exerted pressure, the CE stabilized at around 96.6%, confirming that the pressure can effectively facilitate the plating and stripping process of the lithium metal. The trend of first cycle CE under different stack pressures, at a range of current densities (1.0, 1.5, and 2.0 mA cm⁻²) is also shown in Fig. 4c. It is clear that the stack pressure significantly affects the plating/stripping CE of Li||Cu cells with liquid

electrolytes. The positive effect of stack pressure on Li metal plating/stripping is mainly caused by two reasons: (1) the densification of Li deposits during initial Li nucleation stage; (2) the forced lateral growth of Li metal during Li growth stage.¹¹ Figure 4e also shows the voltage profiles of the anode free Cu||NMC622 full cell with an optimized stack pressure of 350 kPa. It should be noted that such split cell is an open cell design, that may bring concerns about the cycle life in this setup since the amount of liquid electrolyte is limited. As demonstrated in Fig. 4e, the high loading full cell (~4 mAh cm⁻²) can cycle more than 80 h, which is sufficient for fundamental studies for pressure effect on Li metal anode.

With solid state electrolyte: Fig. 4d further illustrates the pressure effect on the stability of Li plating/stripping with an argyrodite SSE. Li symmetric cells with Li₆PS₅Cl are cycled at 75 μ A cm⁻², with 1 h plating/stripping cycles until short-circuiting is observed. The cell pressed to a stack pressure of 75 MPa was short-circuited before the test began. Because of the low yield strength of Li metal, the creeping of Li under such a high pressure allows it to flow within



Figure 4. (a) Completed pressure control apparatus for lithium metal battery with liquid electrolyte or SSE. (b) The voltage profile of first cycle plating/stripping test of the Li||Cu cells with current a density of 2 mA cm⁻² in high concentration ether-based electrolyte: 4.6 m LiFSI + 2.3 m LiTFSI in DME. (c) The trend of first cycle CE under different stack pressures, at current densities of 1.0, 1.5, and 2.0 mA cm⁻², all plated for 4 mAh cm⁻² and stripped to 1 V in a liquid cell.¹² (d) Normalized voltage profiles of Li symmetric cells as a function of time during plating/stripping at different stack pressures in the solid-state cell.¹⁵ (e) The voltage profiles of anode free Cu||NMC622 full cell at rate of C/20 and stack pressure of 350 kPa. (f) The voltage profiles of Li metal | Li₆PS₅Cl | LNO-coated NCA ASSB cycled at rate of C/10 and at a stack pressure of 5 MPa.¹⁵ Reprint permission obtained.

the pores of the SSE, creating an electronic pathway that shorts the cell internally even before any electrochemical testing. When a stack pressure of 25 MPa is applied, the symmetric cell can be cycled for around 48 h before short-circuiting is observed, which is indicated by a sudden drop in the overpotential. It is noteworthy that the cells with stack pressure of 25 MPa and lower only shorts during the plating and stripping process. Similar cycling tests were conducted at stack pressures of 20, 15, and 10 MPa, and similar shorting behavior was observed after 190, 272, and 474 h, respectively. However, at a stack pressure of 5 MPa, no short circuit was observed within 1000 h of the plating and stripping test. All these results show

that Li symmetric cell short-circuiting is both a mechanical and an electrochemical phenomenon. A clear trend can be observed between stack pressure and the time needed before short-circuiting occurs. Furthermore, Fig. 4f presents the voltage profiles of a Li metal | $\text{Li}_6\text{PS}_5\text{Cl}$ | LNO-coated NCA cell cycled at C/10 and with a stack pressure of 5 MPa, at room temperature. The split cell setup can accommodate both the liquid and SSE for Li metal anode. It is believed that while stack pressure is required to provide good initial contact between the electrolyte and the Li by preventing the apparition of voids, a higher stack pressure will also short a cell immediately or after a short time of plating and stripping because of

the creeping of Li metal through the voids in electrolyte under high pressure. Therefore, an optimized stack pressure should also be applied for ASSB cycling.

Conclusions

In summary, a pressure control apparatus is designed for lithium metal batteries with liquid or SSE. The pressure control apparatus consists of one split cell, one load cell, and a metal casing. With high precision machine polishing, the split cell can host liquid electrolytes inside its PEEK die and provide stacking pressure to the electrochemical cell. After careful calibration, the pressure load cell can in situ monitor the pressure exerted on the electrochemical cell with a resolution as high as 0.1 kPa. The apparatus is then used to study the pressure effects on the plating/stripping process in both liquid and solid-state cells. It is shown that the stability of Li plating/ stripping is directly related to the external pressure exerted on the cell. As traditional coin cells become unsuited for studying electrode materials beyond intercalation due to the lack of pressure control, our attempt for designing such experimental cells is early and in no way perfect. We hope to see more creative and elegant designs of experimental cells that allow researchers to reproducibly control the "stack pressure" knob in electrochemistry, in order to obtain meaningful insights on quantitative and reproducible datasets. This work provides guidelines for designing a pressure control setup for Li metal batteries.

Acknowledgments

Funding: This work was supported by the Office of Vehicle Technologies of the U.S. Department of Energy through the Advanced Battery Materials Research (BMR) Program (Battery500 Consortium) under Contract DE-EE0007764.

ORCID

Wurigumula Bao () https://orcid.org/0000-0001-8109-1546 Chengcheng Fang () https://orcid.org/0000-0002-2316-4679 Ying Shirley Meng () https://orcid.org/0000-0001-8936-8845

References

- B. Dunn, H. Kamath, and J.-M. Tarascon, "Electrical energy storage for the grid: a battery of choices." *Science*, 334, 928 (2011).
- J. B. Goodenough and K.-S. Park, "The Li-Ion rechargeable battery: a perspective." J. Am. Chem. Soc., 135, 1167 (2013).

- W. Xu, J. Wang, F. Ding, X. Chen, E. Nasybulin, Y. Zhang, and J.-G. Zhang, "Lithium metal anodes for rechargeable batteries." *Energy Environ. Sci.*, 7, 513 (2014).
- D. Lin, Y. Liu, and Y. Cui, "Reviving the lithium metal anode for high-energy batteries." *Nat. Nanotechnol.*, **12**, 194 (2017).
- C. Fang, X. Wang, and Y. S. Meng, "Key issues hindering a practical lithium-metal anode." *Trends Chem.*, 1, 152 (2019).
- 6. J. Xiao, "How lithium dendrites form in liquid batteries." Science, 366, 426 (2019).
- P. Barai, K. Higa, V. Srinivasan, and L. Berkeley, "Impact of external pressure and electrolyte transport properties on lithium dendrite growth." *J. Electrochem. Soc.*, 165, 2654 (2018).
- H. Lee, S. Chen, X. Ren, and A. Martinez, "Electrode edge effects and the failure mechanism of lithium-metal batteries." *ChemSusChem*, 11, 3821 (2018).
- X. Yin, W. Tang, I. Doo, K. Chai, S. Adams, S. Woo, and G. Wesley, "Nano energy insights into morphological evolution and cycling behaviour of lithium metal anode under mechanical pressure." *Nano Energy*, **50**, 659 (2018).
- A. J. Louli, L. D. Ellis, and J. R. Dahn, "Operando pressure measurements reveal solid electrolyte interphase growth to rank Li-Ion cell performance." *Joule*, 3, 745 (2019).
- C. Fang et al., "Pressure-tailored lithium deposition and dissolution in lithium metal batteries." *Nat. Energy*, 6, 987 (2021).
- L. Gireaud, S. Grugeon, S. Laruelle, B. Yrieix, and J.-M. Tarascon, "Lithium metal stripping/plating mechanisms studies: a metallurgical approach." *Electrochemistry Communications*, 8, 1639 (2006).
- H. J. Chang, N. M. Trease, A. J. Ilott, D. Zeng, L. Du, A. Jerschow, and C. P. Grey, "Investigating Li microstructure formation on Li anodes for lithium batteries by in situ 6 Li/7 Li NMR and SEM." J. Phys. Chem. C, 119, 16443 (2015).
- J. Cannarella and C. B. Arnold, "Stress evolution and capacity fade in constrained lithium-ion pouch cells." J. Power Sources, 245, 745 (2014).
- J. M. Doux, Y. Yang, D. H. S. Tan, H. Nguyen, E. A. Wu, X. Wang, A. Banerjee, and Y. S. Meng, "Pressure effects on sulfide electrolytes for all solid-state batteries." *J. Mater. Chem. A*, 8, 5049 (2020).
- D. P. Wilkinson, H. Blom, K. Brandt, and D. Wainwright, "Effects of physical constraints on Li cyclability." J. Power Sources, 36, 517 (1991).
- M. Genovese, A. J. Louli, R. Weber, S. Hames, and J. R. Dahn, "Measuring the coulombic efficiency of lithium metal cycling in anode-free lithium metal batteries." *J. Electrochem. Soc.*, **165**, 3321 (2018).
- A. J. Louli, M. Genovese, R. Weber, S. G. Hames, E. R. Logan, and J. R. Dahn, "Exploring the impact of mechanical pressure on the performance of anode-free lithium metal cells." *J. Electrochem. Soc.*, **166**, 1291 (2019).
- A. J. Louli et al., "Diagnosing and correcting anode-free cell failure via electrolyte and morphological analysis." *Nat. Energy*, 5, 693 (2020).
- R. Weber, M. Genovese, A. J. Louli, S. Hames, C. Martin, I. G. Hill, and J. R. Dahn, "Long cycle life and dendrite-free lithium morphology in anode-free lithium pouch cells enabled by a dual-salt liquid electrolyte." *Nat. Energy*, 4, 683 (2019).
- L. Porz, T. Swamy, B. W. Sheldon, D. Rettenwander, T. Frömling, H. L. Thaman, S. Berendts, R. Uecker, W. C. Carter, and Y. M. Chiang, "Mechanism of lithium metal penetration through inorganic solid electrolytes." *Adv. Energy Mater.*, 7, 1 (2017).
- J. M. Doux, H. Nguyen, D. H. S. Tan, A. Banerjee, X. Wang, E. A. Wu, C. Jo, H. Yang, and Y. S. Meng, "Stack pressure considerations for room-temperature allsolid-state lithium metal batteries." *Adv. Energy Mater.*, 10, 1 (2020).
- J. Alvarado et al., "Bisalt ether electrolytes: a pathway towards lithium metal batteries with Ni-rich cathodes." *Energy Environ. Sci.*, **12**, 780 (2019).